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# **Hyperdispersion Grating Arrangements for Compact Pulse Compressors and Expanders**

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# Hyperdispersion grating arrangements for compact pulse compressors and expanders

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**Abstract:** A novel, but general, arrangement of parallel sets of gratings is presented that can effectively increase the dispersion of pulse compressors and expanders by over an order of magnitude. These arrangements will dramatically reduce the footprint of the pulse compressors and expanders used in CPA.

## 1. Introduction

Chirped pulse amplification (CPA) [1] is a well-established technique for generation of high-intensity picosecond and femtosecond pulses. In CPA, grating arrangements are used to stretch pulses prior to amplification and compress them afterwards. The footprint of CPA pulse compressors and stretchers is proportional to the dispersion of the gratings and to the inverse of the bandwidth of the pulse. For picosecond CPA, compressor-grating separations of several meters are not uncommon. Application of CPA to materials such as Nd:YAG and Nd:YLF, whose bandwidth would limit compressed pulse durations to of order 5 ps or greater, would require impractically large parallel grating separations. In this paper, we will present a novel, but general, arrangement of parallel sets of gratings that effectively increase the dispersion of the pulse compressor by over an order of magnitude. These arrangements will dramatically reduce the footprint of the pulse compressors and expanders used in CPA systems. This will enable the practical application of CPA to common high-gain but narrow-bandwidth media such as Nd:YAG and Nd:YLF, and greatly simplify the generation of transform-limited, ~1-10 ps, high-energy pulses for precision micromachining, x-ray generation, and lidar, etc.

## 2. Compressor Example

Shown in Fig.1 is a generic arrangement of the hyperdispersion compressor. In this device, nested pairs of parallel gratings are used. The second grating of the configuration amplifies the angular dispersion of the first grating. The third and fourth gratings recollimated the



Figure 1 Generic arrangement for hyperdispersion compressor. At 1.053  $\mu\text{m}$ , for 1760 groove/mm gratings with the separation between the second and third gratings of 1-m and incidence angles of 63°, it is possible to achieve a GDD of  $-1.336 \times 10^7 \text{ fs}^2$ . For comparison, using the same gratings and incidence angles, a standard two-grating Treacy compressor with a separation of 1-m would have a GDD of  $-4.49 \times 10^7 \text{ fs}^2$ .

spectral content and produce a collimated but spatially dispersed pulse spectrum similar to that in a typical Treacy parallel-grating compressor [2]. By double passing the arrangement, the spatial chirp can be removed and the overall separation of the gratings required to produce a particular dispersion is reduced by a factor of 2. Because of the amplified angular dispersion produced by the first two grating elements, the overall footprint (effective grating separation) of this device can be more than an order of magnitude less than a conventional two-grating Treacy compressor with the same dispersion. The principle drawback of this configuration is throughput, since the pulse experiences diffraction from 8 grating surfaces. However, recent advances in multi-layer dielectric (MLD) grating designs can produce diffraction efficiencies in excess of 99% [3], see Fig.2.

## 3. References

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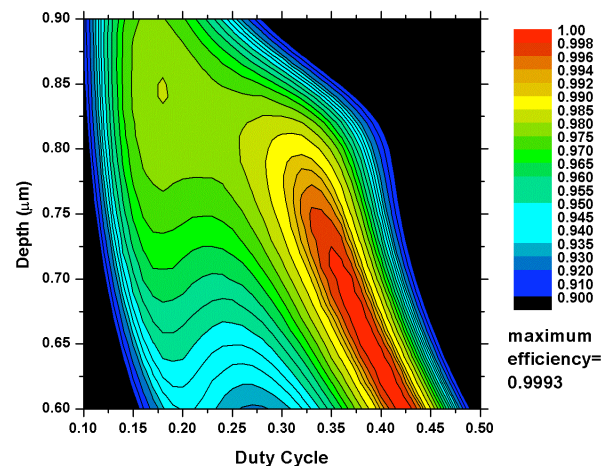


Figure 2 Diffraction efficiency versus groove depth and duty cycle for modern MLD grating design.